## THE EFFECT OF THE VANADIUM CONTENT ON THE MICROHARDNESS OF CoCrFeNiMnV<sub>x</sub> HIGH-ENTROPY ALLOYS IN THE TEMPERATURE RANGE OF 77-293 K <u>H. V. Rusakova<sup>1</sup></u>, L. S. Fomenko<sup>1</sup>, S. V. Lubenets<sup>1</sup>, M. A. Tikhonovsky<sup>2</sup>, I. P. Kislyak<sup>2</sup>, E. D. Tabachnikova<sup>1</sup>, Yi Huang<sup>3</sup>, and Terence G. Langdon<sup>4</sup>

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## ABSTRACT

The main purpose of this work was to investigate the micromechanical properties of CoCrFeNiMnV<sub>x</sub> (x = 0, 0.25, 0.4, 0.5, 0.75, 0.85, 1.5, 2.0) high-entropy alloys in the coarse-grained state at temperatures of 77-293 K.

Dependences of Vickers microhardness on temperature  $H_V(T)$  were obtained for all mentioned alloys except the alloy with x = 2 for the reason of its brittleness. The microhardness of the sigma phase at T = 293 and T = 77 K is about 9.5 GPa and 12.5 GPa, respectively.

**1. THE HOMOGENEITY OF THE SAMPLE STRUCTURE** 



number	size n	mean Ĥ <sub>V</sub> [GPa]	deviation s <sub>d</sub> [GPa]	of the mean s <sub>e</sub> [GPa]	variation <sup>sa</sup> सि <sub>v</sub> [%]
1	85	5.824	0.716	0.078	12.2
2	75	5.707	0.741	0.086	13.0

The microhardness of the two-phase CoCrFeNiMnV<sub>0.85</sub> alloy was measured along two parallel straight lines (axis z in Fig. 1). The distance between these lines was about 1.5 mm, and the distance between the indentations was  $\Delta z = 0.15$  mm. It is evident from Table 1 and Fig. 1 that the values of average (sample mean) microhardness calculated by 85 prints for line 1 and by 75 prints for line 2 are very close to each other, which is facilitated by the large sample size and indicates the macrohomogeneity of the CoCrFeNiMnV<sub>0.85</sub> alloy sample.

<u>Table 1</u>. Sample microhardness characteristics of CoCrFeNiMnV<sub>0.85</sub> HEA, n is the number of measurements of the  $H_V$  value.



## 2. THE INFLUENCE OF TEMPERATURE AND VANADIUM CONTENT ON THE MICROHARDNESS OF ALLOYS CoCrFeNiMnV<sub>x</sub>

CoCrFeNiMnV<sub>0.25</sub> alloy is mainly singlephase with FCC crystal lattice. With temperature decrease from 293 K to 77 K the microhardness of CoCrFeNiMnV<sub>0.25</sub> alloy monotonically increases by about 45% (Fig. 2a) that indicates the thermally activated character of plastic deformation of the material under the indenter.

The CoCrFeNiMnV<sub>1.5</sub> alloy is also mainly single-phase one with a tetragonal lattice, and the whole volume of the alloy is mainly intermetallic sigma phase. The value microhardness of of CoCrFeNiMnV<sub>1.5</sub> alloy increases monotonically by about 32% with temperature decrease from 293 K to 77 K (Fig. 2c).

A completely different behavior of microhardness was observed in the case of the two-phase alloy CoCrFeNiMnV<sub>0.85</sub>. From Fig. 2b it is evident that in a wide temperature range (150-293 K) the average microhardness remains practically unchanged.



At  $x \leq 0.25$  the lattice basically remains FCC, and the microhardness changes slightly with increasing x. However, with a further increase in the vanadium content the formation of a new phase, the intermetallic sigma phase with a tetragonal lattice, takes place. The new hard precipitates act as athermal barriers to the motion of dislocations. A sharp increase in the microhardness, starting from  $x \sim 0.5$ , is due to an increase in the volume fraction of the sigma phase from  $\sim 20$  % up to approximately 100 % in alloys with x = 1.5-2.

**Fig. 2**